

A detailed analysis of eight of the most popular currently available servos from British and Foreign manufacturers

S most digital R/C systems are now compatible it has become fairly A smost digital to experience are now companion of different manufacture in order to achieve a desired performance.

So that an assessment of different servos could be made we contacted all the UK manufacturers and importers in order to obtain samples of servos which they are currently offering. The servos submitted fell into three groups, Group 1 is the 'standard' range not standard as opposed to deluxe but a similar physical size. Eight servos which are the subject of this review were tested. The second group are the mini type and the third-retract, which will be the subjects of future reports.

In order to assess the performance of the servos they were all fed with a similar input from a pulse generator to represent the output of a Tx at an average frame rate calculated from known figures of the most popular systems available at the moment. It must be stressed that all servos were tested to the same signal and it is possible that their performance could be

improved by correction to their particular system timings.

The signal used was 1-2 ms at 18 ms frame time. Bearing in mind the statement in the previous paragraph variations in frame times were tried. In all cases results showed no significant variation in performance

In order to test the servos they were mounted on our standard test rig, a device which only puts a tortional load on the servo about its output axis which is in turn coupled to a cam corrected precision potentiometer. This in turn is fed to an Ultra-Violet recorder which records the rotation of the potentiometer onto a paper trace. This can then be analysed and a true read-out of the rotation against time of the servo can be seen

Several points should be taken into account when reading these results. Firstly, we have yet to see a servo which rotates at the same speed in both directions. This is usually due to the motor, but in some cases the output drive stages of the amplifier. This is relatively unimportant as long as the difference is not too significant. Secondly, the rotation against input pulse length – in a perfect servo this would be absolutely linear. There are two things which govern this linearity.

1. The accuracy of the feedback pot; which in most servos is only of commercial quality and accuracy. Some manufacturers do select these. The inbuilt servo amplifier comparator monostable. Most of the early i.c. amplifier chips suffered in the second category in having restricted monostable ranges which are very non linear outside these restrictions. It would appear that the latest set of i.c. amplifiers now on the market and as used in the eight tested servos have largely overcome this problem.

It is felt that if a 5 per cent error in position accuracy of the servo can be achieved it is quite satisfactory. Note, I say in the servo – overall system accuracy can be as bad as 15 per cent.

Turning to the physical aspects of the servos, i.e. gearboxes appeal etc. then without a doubt the Japanese servos are way ahead of any others on the market. Before anyone accuses me of being anti British I would add that the initial tooling costs to achieve this mechanical standard could just not be justified by a British manufacturer as the worldwide markets are to a great extent beyond the promotional reach of British manufacturers. Let us hope this situation will improve.

The main assets of the Japanese mechanics are the gearboxes, which start off with small gear tooth sizes at the high speed end of the train and increase towards the output end – rather like the gears in a watch are

graded

In all cases (except one) we have given the gearbox details as well as the overall ratio. It is significant to note that they vary quite noticeably for the same stalled torque, except the MacGregor which has a lower ratio by some 20 per cent, yet still achieves a comparable stalled torque. We would assume it to be an efficient electronics/gearbox combination.

Amplifier performance on the whole has greatly improved and indeed the best two amplifiers tested in the group are up to discrete amplifier standard, others fall far behind. It would appear that under the higher load parts of the torque tests the output stages of the amplifiers are coming out of saturation when only subjected to small error signals. This has always been a problem with the i.c. amplifier, but as stated two types seem to have got it sorted out.

The significance of the problem is that if the servo never quite gets to the requested position (due to this droping out of saturation) then under high loads the servo will sit just short of target drawing a lot of current,

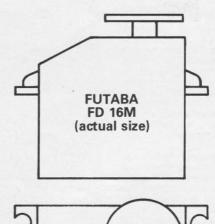
getting hot and running down the batteries.

Now for the results - input signal to all servos 1-2 ms at 18 ms frame rate, +ve pulse.

Servo No. 1 Futaba FD 16M

Load in	Times actu	al in secs	±35°		
oz/in.			Against load	With load	
0	.5	.475	.403	.383	
2	.525	.425	.423	.342	
4	.55	.425	.443	.342	
4 8	.613	.4	.493	.322	
12	.7+.15	.4	.564+.12	.322	
16	.85+.25	.337	.68+.2	.272	
Just stalled l	load 27 oz/in. To	otal travel 93	30	1 ms=47°	
				$2 \text{ ms} = -46^{\circ}$	

Amplifier 2 i.c.'s type BA 606 and BA 607A Gearbox ratio's 10T-50T 12T-50T 10-38 12-36 output square Total ratio 239:1 Motor type (unmarked)



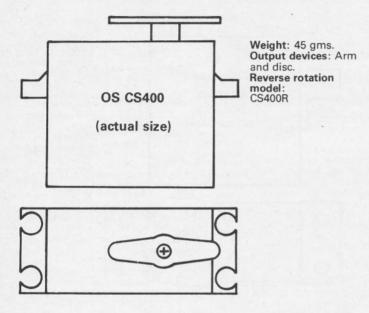
Weight: 44 gms. Output devices: Long and short arms. Drilled and plain discs. T' arm. Reverse rotation

model: Label colour different.



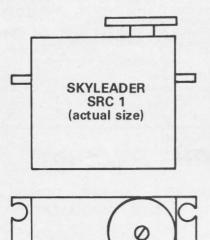
Servo No. 2 OS CS400

Load	Time actua	l in secs		±35°	
oz./in.	Against load		nd Agains	t load Wi	ith load
0	.362	.364	.28	.26	,
0 2 4 8 12	.434	.35	.31	.25	
4	.462	.322	.33	.23	
8	.602	.308	.43	.22	
12	.756	.308	.54	.22	
16	1.33	.244	.94	.21	
Just stalle	d load 20 oz./in.	Total tra	vel 105°		$1 \text{ ms} = +51^{\circ}$
					$2 \text{ ms} = -54^{\circ}$
Amplifier	XR 1 off i.c. 226	2CP			
Gearbox	Motor 1 Overall ratio 1:	1T-55T 58:1	14T-42T	14T-42T ot	12T-42T utput splined
Motor typ	e 16 mm unmark	ted			



Servo No. 3 Skyleader SRC 1

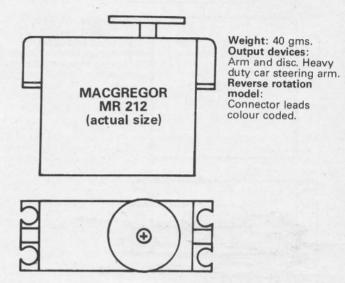
Load	Time actu	al in secs	±3	35°
oz/in.	Against load	With load	Against load	With load
0	.45	.425	.351	.33
2	.475	.4	.371	.31
4	.5	.4	.390	.31
0 2 4 8 12	.55	.375	.430	.292
12	.625+.2	.35	.488+.16	.277
16	.7+.15	.35	.547 + .12	
Just stalle	d load 28 oz./in.	Total travel	96°	$1 \text{ ms} = 50^{\circ}$
				$2 \text{ ms} = -46^{\circ}$
Amplifier	SRC 419P+2 tra	nsistors		
	Motor 8		Г-40Т 9Т-40	T 16T-40T
Overall ratio 242:1		Outpu	t conical serrated	
Motor:- N	Iitsumi		Outpu	t comean serrated



Weight: 40 gms. Output devices: 1 arm. Large and small disc. Reverse rotation model: Colour spot on case. Interchangeable rack or rotary output.

Servo No. 4 MacGregor MR 212

Load in	Time actu	Time actual in secs		35°
oz./in.	Against load	With load	Against load	With load
0.	.4	.388.	.291	.282
0 2 4 8 12	.45	.388	.327	.282
4	.475	.375	.346	.273
8	.525	.375	.382	.273
12	.6	.350	.436	.254
16	.75	.350	.546	.254
	d load 27 oz./in.			$1 \text{ ms} = +58^{\circ}$ $2 \text{ ms} = -55^{\circ}$
Amplifier	DIL unmarked +	-2 transistors		
Gearbox	Motor 8 Overall ratio 20		Г-38Т 10Т-3	8T 12-36
Motor typ	e 16 mm			

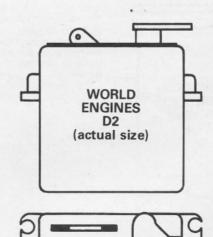


Servo No. 5 World Engines D2

Load in	Time act	Time actual in secs		5°
oz./in.	Against load	With load	Against load	With load
0	.338	.325		
0 2 4 8 12	.375	.313	Actua	al rotation
4	.413	.308	ider	ntical to
8	.525(+.09)			ted rotation
12	.78(+.4)		001100	ed rottinon
Just stalled load 14 oz./in. Total travel 70°			70°	$1 \text{ ms} = +32^{\circ}$
				$1 \text{ ms} = -37^{\circ}$
Gearbox o	verall ratio 205:	1)		

Amplifier 1 off NE544 i.c. Motor type Furuichi 16 mm.

figures quoted by manufacturer



Weight: 38 gms. Output devices: 'T' arm, straight arm. Reverse rotation model:

Colour spot on case.

Servo No. 6 Linward 13M (SLM ball bearing mechanics).

Load in	Times actu	al in secs	±35°	
oz./in.	Against load	With load	Against load W	ith load
0	.375	.3	.319	.256
2	.475	.275	.404	.344
4	.65+.1	.25	.554+.08	.213
6	1.375	.25	1.17	.213
0 2 4 6 12 16 STAL	LED. Never go	t to desired	position	
	d load 7.5 oz. To	otal travel 89	90	1 ms=47°
				$2 \text{ ms} = -42^{\circ}$
Amplifier .	Signetics NE 54	4N		
	Motor 1		T-36T 10T-36T	17T-42T
Note outpo	ut gears are of n Overall ratio 1		llbearings on outp	ut shaft.

Weight: 55 gms.
Output devices:
Long and short offset
arms. 'T' arm. Single
side arm. Retract type
arm.

Servo No. 7 Sprengbrook

Load in oz./in.	Times actu Against load		Against load	
0	.4	.38	.341	.33
0 2 4 8 12	.45	.375	.383	.319
4	.475	.362	.405	.308
8	.55	.35	.469	.298
12	.575+.17	5 .35	.490+.14	9 .298
16	.65+.35	.35	.553+.29	8 .298
Just stalled	I load 27 oz./in.	Total travel	88°	1 ms=41° 2 ms=47°
Amplifier 2	2 i.es. DIL			
	Motor 10 Overall ratio 20		OT-38T 10T-38	3T 10T-38T

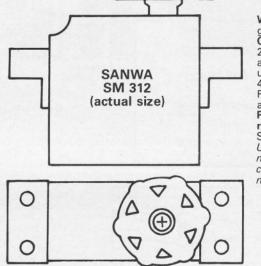


Weight: 45 gms. Output devices: Disc 3 lengths of arm. Reverse rotation model: Label identification.

Reverse remodel: Label iden | Size |

Servo No. 8 Sanwa SM312

Load in	Times actu	Times actual in secs		5°
oz./in.	Against load	With load	Against load	With load
0	.537	.475	.383	.34
2	.562	.475	.401	.34
2 4 8	.592	.45	.423	.32
8	.662	.425	.473	.30
12	.75	.425	.536	.30
16	.85+'.162	2 .413	.607+.12	.29
Just stalled	d load 27 oz./in.	Total travel	113°	1 ms=54° 2 ms=59°
Amplifier i	.c. DIL 2 off on 520-650	e on top of	other.	
Gearbox	Motor 10 Overall ratio 25		T-50T 10T-50	T 19T-38T
Motor type	e 16 mm Mitsum	i		



Weight: 55 gms.
Output devices: 2 sizes 6 way arms. 2 sizes undrilled discs. 4 way arm. Retract type arm.
Reverse rotation model: SM311.
Unique moulded rubber cushion mounts.

At a glance

		Aga	inst load		
Servo	Gear ratio	Max. Pull oz./in.	Fastest speed	Fastest 16-oz.	Motor
Futaba	239:1	27	.403	.68+.2	16mm
O.S.	158:1	20	.28	.94	16mm
Skyleader	242:1	28	.351	.547+.12	16mm
MacGregor	207:1	27	.291	.546	16mm
World Engines	205:1	14	.338		16mm
Linward	116.7:1	7.5	.319		16mm
Sprengbrook	208:1	27	.341	.553 + .298	16mm
Sanwa	250:1	27	.383	.607+.12	16mm

From the 'at a glance' chart it can be seen that no individual servo can claim best results in all areas tested.

The Skyleader has just the edge on max torque but falls far behind, on speed to achieve this result. The OS CS400 comes out the faster on 'No load' and remains linear over the load range but suffers from a large drop-off in speed at the high loads. It would appear that a slightly higher gearbox ratio would improve this servo.

The MacGregor servo gives the best 'under load' speed again without falling out of saturation as does its nearest rival the Skyleader.

Conclusion

From a performance point of view the best all round performance goes to the *MacGregor*. Whether its lack of eye appeal and relatively noisy gearbox put you off is up to you.

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